



Figure 5.10 Absolute liquid slug length *versus* superficial gas velocity: $U_{LS} = 0.030915 \text{ m s}^{-1}$, the superficial liquid velocity used in the crystallizer with coaxial mixing of hot solution with cold liquid; $U_{LS} = 0.015457 \text{ m s}^{-1}$, the superficial liquid velocity used in the crystallizer with radial mixing of hot solution with cold liquid; Reynolds number $Re_L < 2100$.

Table 5.1 Comparison of calculated and experimental liquid slug lengths in crystallizer.

Type of mixer	$U_{LS}, \text{ m s}^{-1}$	$U_{GS}, \text{ m s}^{-1}$	Measured $l_s, \text{ m}$	Predicted $l_s, \text{ m}$
Coaxial	0.030915	0.056442	0.0060	0.00545
Radial	0.015457	0.035209	0.0040	0.00456

(5.14) gives a reasonable estimate of liquid slug length, with some under-prediction for the configuration that had an upstream coaxial mixer and some overprediction for the configuration that had an upstream radial mixer.

Absolute recirculation times τ_{cir} *versus* superficial gas velocity U_{GS} are plotted in Figure 5.11 for the superficial liquid flow rates used for the coaxial and radial mixing experiments.² The values of τ_{cir} decline exponentially with U_{GS} , reflecting the similar decline in slug length.

5.3.2.3 Mixing Efficiency

To estimate the completeness of micro-mixing from the previous calculations, we introduce the micro-mixedness ratio α ,³¹ which is a measure of the perfectly mixed volume to the totally segregated volume in the mixing process. This ratio is defined in terms of a segregation variable X_s , which is 0 for perfect mixing and 1 for complete segregation:

$$\alpha = \frac{1 - X_s}{X_s}. \tag{5.16}$$