

A more general theoretical approach for dissolution modeling called the *Film-Model Theory* was postulated by Nernst (1904) and expanded upon by Brunner (1904) in an effort to deconvolute the components of the dissolution constant, k . Both Nernst and Brunner made the following assumptions:

1. The mass flux, that is, intrinsic dissolution rate, is governed by Fick's first law of diffusion:

$$J = \frac{dm}{dt} \left(\frac{1}{S} \right) = -D \left(\frac{dc}{dx} \right) \quad (17.12)$$

where dc/dx is the solute concentration gradient and D is the diffusivity (diffusion coefficient), and

2. The concentration gradient within the diffusion layer is constant, thus,

$$\frac{dc}{dx} = \frac{(c_t - c_s)}{h} \quad (17.13)$$

where h is the thickness of the stagnant diffusion layer.

Substitution of Equation 17.13 into Equation 17.12 gives

$$J = \left(\frac{dm}{dt} \right) \left(\frac{1}{S} \right) = \frac{D(c_s - c_t)}{h} \quad (17.14)$$

This led to the following equation:

$$\frac{dc}{dt} = k_2 \left(\frac{DS}{Vh} \right) (c_s - c_t) \quad (17.15)$$

where k_2 is the intrinsic dissolution rate constant.

Sink Conditions

Sink conditions refer to a special case where there is essentially no buildup of the solute, which is assumed to be the case for the absorption of a drug from the gastrointestinal tract. Two ramifications for this special case are that the concentration gradient ($c_s - c_t$) described in Equation 17.9 is not rate-limiting under any conditions and, if the surface area of the solute is kept constant, the rate of dissolution will follow zero-order kinetics. *In vivo* sink conditions can be approximated *in vitro* by ensuring that the concentration of the solute does not exceed 5%–10% of its solubility. In practice, this is accomplished by either using a large volume of the dissolution medium or continuously replenishing the dissolution medium under carefully controlled conditions. Under sink conditions, $c_s \gg c_t$, and Equation 17.15 can be rewritten as the limiting case:

$$\left(\frac{dc}{dt} \right)_{t \rightarrow 0} = k_2 \left(\frac{DS}{Vh} \right) c_s \quad (17.16)$$

Since D , c_s , and k_2 are constants for a given solute, they can be combined into k_3 , and Equation 17.16 can be further simplified into

$$\frac{dc}{dt} = k_3 \left(\frac{S}{Vh} \right) \quad (17.17)$$